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# Confinement effects in laminar swirling jets

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This paper explores the effect of axial and radial confinement on the flow topology of laminar swirling jets. Its objective is to provide a unifying perspective toward swirling jet mechanics that connects earlier reports across a variety of confined and unconfined flow situations and over a range of swirl ratio  $S$  values. The analysis focuses separately on the influence of the jet's injection depth  $L$  in a radially-unconfined flow and of the chamber diameter  $C$  in radially-confined jets. In the former case, it shows that axial confinement strongly influences the jet's behaviour when  $L$  is small, allowing bistable steady-states: a central jet (CJ) solution with or without a small central recirculation zone (CRZ), and a wall jet (WJ) solution with a wide-open CRZ spreading along the reservoir's edge. Similar behaviour is identified for radially-confined jets, where bistable CJ and WJ states appear over a range of moderate  $C$  values, and the WJ state adopts a conical CRZ. In either case, the WJ solution appears or disappears via saddle–node bifurcations when the confinement is made sufficiently strong or weak, respectively. This dynamics is attributed to an exchange of dominance between central and outer low pressure regions as the flow transitions from CJ to WJ or vice-versa. The findings demonstrate that the hysteresis widely associated with swirling jets is controlled not just by vortex breakdown, but also by confinement through the Coandă effect. Such confinement is found to significantly alter the state-space structure even when the walls are far from the nozzle.

**Key words:** bifurcation, vortex breakdown, jets

## 1. Introduction

Among the family of canonical shear flows, swirling jets are a remarkable genus with widespread practical and scientific interest. Yet, even in heavily simplified circumstances, swirling jets exhibit a suite of complex behaviours stemming from interactions among centrifugal, Coriolis, and shear forces (Gallaire & Chomaz 2003). Perhaps the best-known of these behaviours is the phenomenon of vortex breakdown, whereby sufficiently strong swirl induces the formation of an internal stagnation point along the axis of columnar vortices. Though it is often introduced as a controversial theoretical issue, the basic mechanics of the vortex breakdown phenomenon is now quite well understood (Brown & Lopez 1990; Wang & Rusak 1997*a*; Gallaire *et al.* 2004), and there is little room for debate about its fundamental

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nature. Even so, the interaction among vortex breakdown and other phenomena is not always intuitive. Indeed, several swirling jet behaviours remain incompletely understood due to confounding influences from significant configurational sensitivities and pronounced nonlinear effects. One such issue pertains to how the central recirculation zone (CRZ) that forms when vortex breakdown occurs interacts with the outer recirculation zone (ORZ) in the entrained fluid surrounding the jet. This interaction, the focus of this paper, will be explored by using bifurcation analysis to connect the jet’s physical behaviours to the properties of its state space.

Before moving on to a more comprehensive discussion of swirling jet behaviours, it is worth briefly recounting the current scientific consensus on the issue of vortex breakdown. The modern theory of vortex breakdown is based on the inviscid and axisymmetric explanation of Wang & Rusak (1997a), which built upon earlier ideas of a supercritical–subcritical flow transition by Squire (1960) and Benjamin (1962). Later extended to three dimensions by Wang *et al.* (2016), this theory describes vortex breakdown as the consequence of a columnar vortex attaining a swirl level where upstream-propagating inertial waves are supported. In such conditions, the backpropagating disturbance waves can interact with streamwise inhomogeneities such as a swirl generator or an expansion to accumulate at a fixed location in space (Gallaire & Chomaz 2004). As these disturbances accumulate, the local pressure gradient eventually becomes insufficient to maintain a columnar equilibrium, and the flow evolves towards a breakdown state with a CRZ (Hall 1972; Brown & Lopez 1990; Gyllenram *et al.* 2007). Beyond the critical swirl level, this breakdown of the columnar flow is spontaneous via infinitesimal perturbations. Yet columnar and breakdown flow states can both exist for a finite interval of below-critical swirl demarcated by a pair of saddle–node bifurcations (Beran & Culick 1992; Lopez 1994). This bistable behaviour gives rise to abrupt, hysteretic flow transitions when the swirl parameter traverses a turning point, and finite-amplitude perturbations may trigger similar transitions within the bistable interval. However, a variety of different influences can modify or eliminate this bistable behaviour. For example, Wang & Rusak (1997b) explained how viscosity “unfolds” the saddle–node bifurcations below a certain Reynolds number, permitting a smooth, non-critical evolution of the steady flow from columnar to breakdown states as the swirl increases (and vice-versa). Similar unfolding behaviour also occurs with certain columnar vortex profiles (Leclaire & Sipp 2010; Zhang *et al.* 2019) and with small divergences of the columnar flow (Rusak *et al.* 1997; Rusak & Judd 2001). Overall, this collection of theory nicely explains many key aspects of the vortex breakdown phenomenon in a wide range of columnar swirling flows (Sarpkaya 1971; Leibovich 1984; Ruith *et al.* 2003; Gallaire *et al.* 2006), including swirling jets (Billant *et al.* 1998; Liang & Maxworthy 2005; Manoharan *et al.* 2020).

Nonetheless, swirling jets exhibit a broad set of behaviours that are distinct from vortex breakdown. For example, a variety of flow instabilities emerge at levels of swirl below the breakdown transition, manifesting various rotating spiral structures concentrated along the jet’s shear layers (Billant *et al.* 1998; Loiseleux & Chomaz 2003; Liang & Maxworthy 2005). Other three-dimensional structures also appear at high swirl alongside breakdown, where they are associated with phenomena such as precessing vortex core (PVC) oscillations (Syred 2006; Oberleithner *et al.* 2011; Tammisola & Juniper 2016; Manoharan *et al.* 2020). Besides these unsteady behaviours, significant changes in swirling jets’ steady or time-mean flow structure are also possible beyond vortex breakdown. Such transitions typically involve notable changes in the size and shape of the CRZ and ORZ. For instance, the small central recirculation “bubble” may abruptly and dramatically expand into a significantly larger volume with a windward streamsurface that is either cone-shaped (Jiang & Shen 1994; Billant *et al.* 1998; Liang & Maxworthy 2005) or flattened along an axial wall (Vanierschot & van den Bulck 2007; O’Connor & Lieuwen 2012; Ogus *et al.* 2016). In either case, the

literature widely notes a measurable range of hysteresis in the swirl parameter between flow states with small ellipsoidal CRZs and those with conical or flattened ones.

In a recent pair of studies led by the first author, bifurcation analysis was used to investigate the steady and time-periodic dynamics of radially unconfined laminar swirling jets issuing from rotating pipes mounted flush against a semi-infinite axial wall (Douglas *et al.* 2021, 2022). Those studies demonstrated that, in the steady regime, an axisymmetric CRZ emerges gradually in the quasicolumnar jet due to vortex breakdown as the swirl ratio is increased. They also showed that unsteady and non-axisymmetric features and subcritical dynamics became important to the overall vortex breakdown process as the Reynolds number increased. An important detail of these studies was the characterisation of bistable central jet (CJ) and wall jet (WJ) states reminiscent of the hysteresis behaviour previously observed in annular swirling jets (Vanierschot & van den Bulck 2007; Ogus *et al.* 2016). In line with an analysis by Vanierschot & van den Bulck (2009), Douglas *et al.* (2021) argued that these transitions occurred due to an exchange of dominance between low pressure regions in the CRZ and ORZ. However, these papers did not analyse the mechanics of this process in detail, and did not explore how the characteristics of the post-breakdown transition could be influenced by the axial wall's position or by the inclusion of a radial wall. Such geometric effects are important to understand, as prior investigations have established that swirling flows are remarkably sensitive to confinement (Ruith *et al.* 2004; Fu *et al.* 2005), and large-scale changes in the topology of the CRZ and ORZ can have serious consequences in confined applications such as swirl-stabilised combustors (Fritz *et al.* 2004; Lieuwen *et al.* 2008; Mohammad *et al.* 2011). Thus, the main purpose of this article is to explore how confinement influences the state space dynamics underlying the nonlinear transitions between CJ and WJ states. Additionally, it aims to elucidate the physical processes that control the structure of strongly swirling jets' CRZ and ORZ.

The remainder of this paper is organised as follows. Section 2 describes the flow configuration and outlines the numerical methodology. Section 3 presents the main results and begins by considering the role of the injection depth in a radially-unconfined flow in section 3.1. Similar analyses toward the effect of radial confinement and the Reynolds number are then given in sections 3.2 and 3.3, respectively. Finally, our main conclusions are summarised and contextualised within the existing literature in section 4.

## 2. Problem formulation

### 2.1. Flow configuration

The present flow configuration is based on earlier work by Douglas *et al.* (2021) studying radially-unconfined, flush-mounted swirling jets and is inspired by the experimental setup of Billant *et al.* (1998). As shown in figure 1, the configuration features a fully-developed, constant-density flow with a volume-averaged velocity  $U$  expanding from a long rotating pipe of diameter  $D$  into a large axisymmetric reservoir. We consider two situations: (1) an unconfined case where the reservoir is unbounded in the radial direction and (2) a confined case where a cylindrical wall bounds the radial extent of the domain. Using  $U$  and  $D$  as velocity and length scales, we define the Reynolds number  $Re = UD/\nu$ , based on the fluid's constant kinematic viscosity  $\nu$ , and the kinematic swirl ratio  $S = \frac{1}{2}\omega D/U$ , based on the pipe's rotation rate  $\omega$ . In addition, the injection depth and chamber diameter parameters, respectively  $L \geq 0$  and  $C \geq 1$ , are defined based on the dimensions of the reservoir as indicated in figure 1. Note that  $C$  will be taken as infinite for the unconfined case. In either case, the fluid motion is characterised by the velocity  $\mathbf{u}$  and pressure  $p$  fields, which evolve

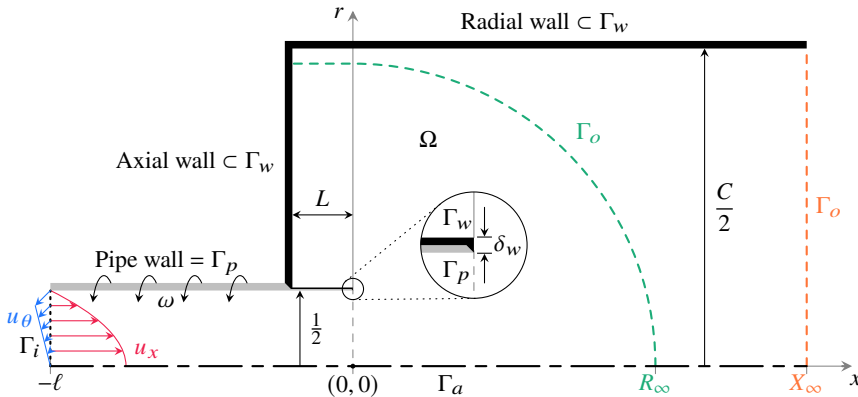


Figure 1: Meridional plane schematic of the flow configuration (not to scale). For the unconfined and confined cases,  $\Gamma_o$  is denoted by the green and orange labels, respectively.

inside the domain  $\Omega$  according to the incompressible Navier-Stokes equations,

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p + Re^{-1} \nabla^2 \mathbf{u}, \quad (2.1a)$$

$$0 = \nabla \cdot \mathbf{u}. \quad (2.1b)$$

To model the configuration described above and in figure 1, the following constraints are enforced along the domain boundaries. The long rotating inflow pipe is truncated to a length  $\ell$ , and an upstream boundary  $\Gamma_i$  is introduced. There, a fully-developed rotating Poiseuille flow is imposed with Dirichlet conditions for the axial and azimuthal velocity components and a Neumann condition for the radial component. Along the rotating pipe wall  $\Gamma_p$  and the static reservoir walls  $\Gamma_w$ , Dirichlet conditions enforce no-slip velocity constraints. Note that the protruding pipe has a finite wall thickness of  $\delta_w = 10^{-5}$ , which was used to spatially distinguish between  $\Gamma_p$  and  $\Gamma_w$ . Following a Fourier expansion along the azimuth into integral wavenumbers  $m$ , three-dimensional symmetry conditions are enforced for the velocity along the central axis  $\Gamma_a$ . Finally, the outgoing flow from the reservoir is modelled by truncating the domain to a radius of  $R_\infty$  for the unconfined case or a length of  $X_\infty$  for the confined case. The centrifugally-balanced directional outflow condition developed in Douglas *et al.* (2021) is then enforced along the corresponding outflow boundary  $\Gamma_o$ . Note that, in the  $x \rightarrow \infty$  limit, the velocity in the reservoir without truncation will vanish in the unconfined case or develop to a non-rotating Poiseuille profile in the confined case.

## 2.2. Solution methodology

The discretisation approach leveraged in this work is essentially identical to that of Douglas *et al.* (2021), with the only notable distinction being related to the treatment of the injection depth and chamber diameter parameters. All calculations are performed on generic meshes in computational coordinates that are piecewise linear functions of the physical coordinates. This avoids requiring unique meshes for each discrete geometry and, instead, imbues the variational formulation with a continuous dependence on  $L$  and  $C$ . The primary computational meshes consist of Delaunay triangulations of  $\Omega$  in the meridional plane involving  $\sim 160\,000$  elements in both the unconfined and confined cases. These meshes are characterised by the dimensions  $\ell = 4$ ,  $R_\infty = 40$ , and  $X_\infty = 100$ . Certain calculations were also repeated on additional meshes of varying dimension and resolution to ensure mesh independence. Finally, the formulation is projected onto the basis of Taylor–Hood ( $\mathbb{P}_2 \times \mathbb{P}_1$ ) finite elements

associated with the meshes using FreeFEM (Hecht 2012), resulting in discrete flow states with a total of  $\sim 1.1$  million degrees of freedom in the meridional plane.

The present solution techniques are also duplicated from Douglas *et al.* (2021), and readers are referred to that work for details. To summarise, (2.1) is rewritten in state-space form as,

$$\mathcal{M} \partial_t \mathbf{q} + \mathcal{R}(\mathbf{q}) = 0, \quad (2.2)$$

where  $\mathcal{M}$  and  $\mathcal{R}$  are the respective mass matrix and residual operators and  $\mathbf{q} = (\mathbf{u}, p)^T$  is the state vector. Nonlinear parameter continuation methods based on a Moore–Penrose predictor-corrector scheme are used to extract branches of steady solutions that satisfy,

$$\mathcal{R}_0(\mathbf{q}_0) = 0, \quad (2.3)$$

where the 0-subscript denotes axisymmetry. Eigenvalue calculations are used to ascertain the stability of these steady states to infinitesimal three-dimensional disturbances of the form,  $\hat{\mathbf{q}}_m(x, r) \exp[im\theta + (\sigma + i2\pi f)t]$ , where  $\sigma$  is the linear growth rate and  $f$  is the frequency. In this paper, we take  $m \leq 0$  without loss of generality such that for  $m \neq 0$ ,  $f > 0$  and  $f < 0$  indicate perturbations that, respectively, co-rotate and counter-rotate with respect to the pipe’s rotation direction. Such perturbations obey the linearised system,

$$(\sigma + i2\pi f) \mathcal{M} \hat{\mathbf{q}}_m + \mathcal{J}_m(\mathbf{q}_0) \hat{\mathbf{q}}_m = 0, \quad (2.4)$$

where  $\mathcal{J}_m$  is the Jacobian operator. Hence, local bifurcation points occur at parameter values where (2.3) and (2.4) are satisfied under the criticality condition  $\sigma = 0$ .

### 3. Results and Discussion

#### 3.1. Axial confinement effects

We begin our presentation of results with an investigation into the influence of the injection depth ( $L$ ) on the behaviour of the radially unconfined swirling jet at  $Re = 100$ . This  $Re$  value is sufficiently low to suppress any oscillatory instabilities within the investigated portion of the radially unconfined parameter space, while still allowing the nonlinear behaviours of interest to occur amongst the axisymmetric steady states as  $S$  and  $L$  are varied. The results of the analysis are presented in the bifurcation diagrams and flow visualisations of figure 2, which synthesise data obtained from approximately 2700 discrete steady state and eigenvalue calculations. Here, as in several earlier studies (e.g. Beran & Culick 1992), the evolution of the CRZ is monitored on the bifurcation diagrams by extracting the minimum of the axial velocity along the centerline,  $\min u_x(x, 0)$ , from each solution.

The diagrams in figures 2(a) and (b) reveal a notable change in the behaviour of the swirling jet as the injection depth is varied. For flush injection ( $L = 0$ ), figure 2(a) recovers the bifurcation diagram already studied by Douglas *et al.* (2021). Here, bistable behaviour associated with a pleated pair of saddle–node bifurcations along  $S$  occurs between a stable branch of CJ solutions (similar to the streamline visualisations in figure 2(c) or figure 2(d) point 2) and a stable branch of WJ solutions (similar to the visualisations in figure 2(d) point 4 or figure 2(e)). As the injection depth is increased, however, this behaviour changes with the corresponding reduction in the axial wall’s influence. For example, at  $L = 1$ , the CJ solution curve in figure 2(a) exhibits no saddle–node bifurcations along  $S$ , such that the WJ solution curve is disconnected from the CJ curve. This indicates that, within the bistable interval of  $S$ , a large-amplitude perturbation to the CJ is required for the system to transition to a WJ state – this transition cannot occur spontaneously by smooth variations of  $S$ . (Visualisations of the stagnation streamlines associated with these bistable states, as well as their intermediate saddle solution, are overlaid in figure 2(d) for points 2-4.) Furthermore, beyond a sufficiently

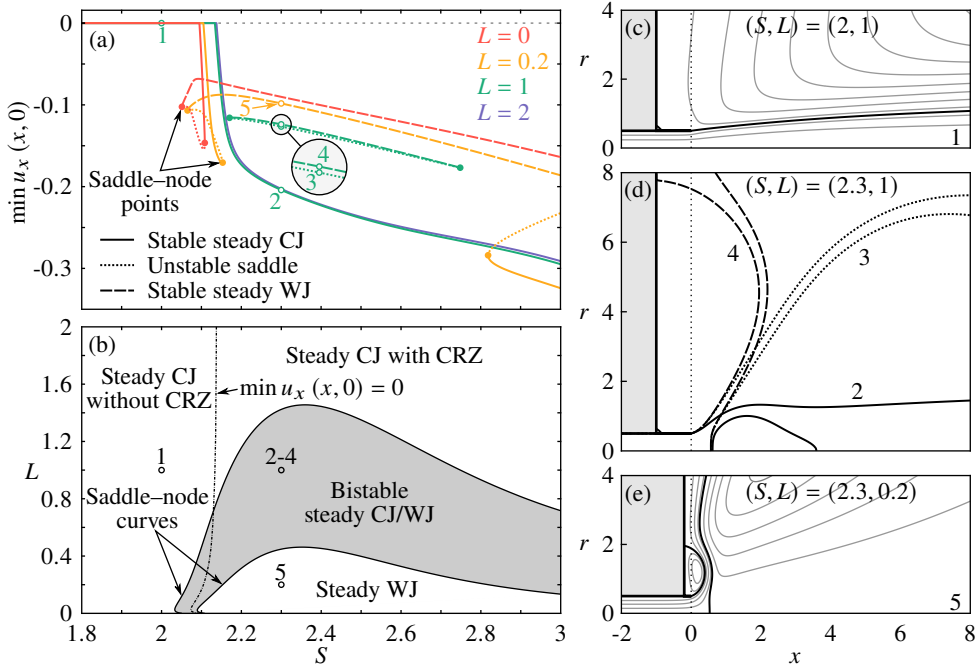


Figure 2: (a) Bifurcation diagrams, (b) stability map, and (c-e) streamline visualisations illustrating the effect of varying the injection depth and swirl ratio for the radially unconfined configuration at  $Re = 100$ . Visualisations correspond to the points labelled in the diagrams. Note that only a small portion of the overall computational domain is shown.

high value of  $L$  (corresponding to  $L \approx 1.5$  at this Reynolds number), the WJ solution ceases to exist entirely. For such large  $L$  values, the CRZ grows uniformly in size and intensity as  $S$  increases beyond the  $\min u_x(x, 0) = 0$  threshold along a monostable CJ solution curve.

As mentioned in the introduction, the bistable behaviour between CJ and WJ solutions observed in figure 2 is distinct from the basic vortex breakdown phenomenon. Indeed, Vanierschot & van den Bulck (2009) have explored such bistable behaviour and outlined some of the physical mechanisms at play as the flow transitions between states. Earlier work by the lead author has also shown that such bistable behaviour results from an exchange of dominance between low pressure regions located within the CRZ and the ORZ based on analysis of the critical eigenmodes associated with the saddle–node bifurcations (Douglas *et al.* 2021). Regardless, in our opinion, the literature is still lacking a general explanation of the fundamental physical processes underlying the transition between CJ and WJ states. As such, the following paragraphs serve to develop an intuitive physical interpretation of the observed flow transitions. The proposed model explains these transitions as the outcome of a competition between central and outer low pressure regions whose dominance is controlled primarily by two competing processes.

The first of these basic processes arises from intrinsic interactions between the centrifugal force and pressure gradient in an axisymmetric swirling flow. This process has been thoroughly studied by Brown & Lopez (1990), and the reader is referred to their work for additional rigour and more complete details. Nonetheless, the main points are summarised here. In an inviscid columnar vortex, the centrifugal force must be balanced by a monotonic, outward-oriented radial pressure gradient, yielding a pressure deficit along the axis. This equilibrium between the pressure gradient and the centrifugal force must be overcome for

vortex breakdown to appear (Hall 1972; Gyllenram *et al.* 2007). However, once  $S$  becomes large enough to break radial equilibrium and spur vortex breakdown, the fluid's azimuthal velocity must decrease as it diverges from the centreline in order to conserve angular momentum. This reduction in azimuthal velocity, in turn, weakens the centrifugal force. Consequently, the diverging flow eventually reaches a position where the radial pressure gradient locally overpowers the centrifugal force (i.e. where  $\partial p/\partial r > u_\theta^2/r$ ). This causes the stream to curve back towards the axis, yielding the classical “bubble” shape of the CRZ following vortex breakdown in many examples. The upshot is that this process always acts to *decrease* the size of the CRZ, thereby also acting to *increase* the size of the ORZ.

The second effect, in contrast, is related to extrinsic interactions of the jet with confinement, resulting in a pressure deficit along the boundaries. This pressure deficit arises through the Coandă effect, whereby a wall restricts entrainment, disproportionately accelerates the entrained fluid near the wall, and accordingly decreases the local static pressure. This general phenomenon, which has been extensively investigated in swirling annular jets by Vanierschot & van den Bulck (e.g. 2007, 2009), results in an attractive force pulling the jet towards the wall. Moreover, the magnitude of this attractive force increases as the confinement intensifies, introducing an important nonlinear mechanism for hysteresis. Since the walls in a circular jet are all located radially outside of the jet, the Coandă effect always acts to *decrease* the size of the ORZ. Thus, it must also *increase* the size of the CRZ when it is present. However, it is interesting to note that in an annular jet configuration, the Coandă effect also produces a force pulling inwards towards the centrebody.

As explained above, the pressure gradients resulting from the centrifugal effect and from the Coandă effect always act in opposite directions in circular swirling jets. We propose that these two competing effects are sufficient for a straightforward interpretation of the bifurcation scenario. If the former dominates, vortex breakdown may cause flow stagnation, but the low central pressure acts to promptly close the CRZ as long as the centrifugal pressure gradient remains dominant. In this case, confinement has a weak effect, and the flow retains a CJ structure with a large ORZ. Conversely, if the Coandă effect dominates, the low pressure resulting from entrainment in the ORZ pulls the jet strongly towards the confining walls to yield a WJ structure. This opens up the CRZ into a bigger volume with a shape largely determined by the geometry of the reservoir. Overall, this interpretation of competing effects allows a physically intuitive and qualitatively accurate understanding of the results in figure 2. The monostable CJ and WJ regimes in figure 2(b) are each characterised by a decisive dominance of one of the two effects. Conversely, the bistable regime occurs when the two influences may be of comparable magnitude for a given set of boundary conditions, such that the dominant influence is selected by the particular initial conditions.

Another interesting aspect of figures 2(a) and (b) concerns how the threshold  $S$  required for a central stagnation point to form increases slightly with increasing  $L$ . We interpret this observation in terms of the theoretical explanation of vortex breakdown reviewed in the introduction. Namely, as the secondary flow in the reservoir becomes more aligned with the jet stream along the injection plane with increasing  $L$ , the enhanced axial co-flow limits the ability of disturbances to propagate upstream. Simultaneously, flow alignment reduces the pressure drop across the expansion, homogenising the flow along the streamwise direction. Both of these effects are known to make vortex breakdown globally less favourable in inviscid swirling pipe flows (Gallaire & Chomaz 2004), suggesting that these same influences forestall stagnation to higher  $S$  conditions at higher  $L$  values in the viscous swirling jet considered here.

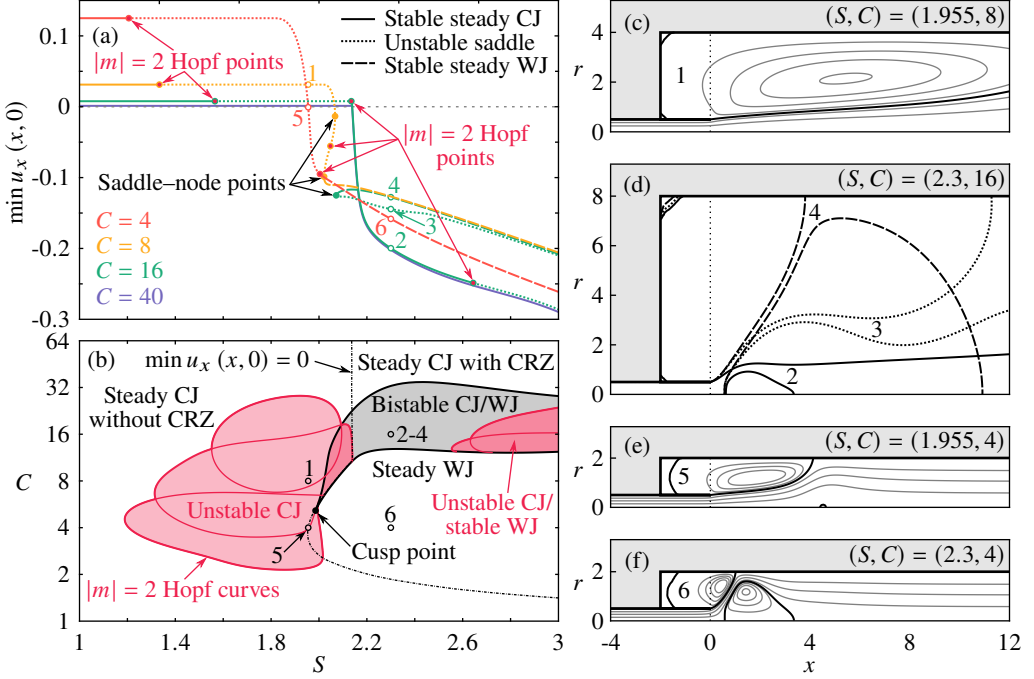


Figure 3: (a) Bifurcation diagrams, (b) stability map scaled logarithmically in  $C$ , and (c-f) streamline visualisations illustrating the effect of varying the chamber diameter and swirl ratio with weak axial confinement ( $L = 2$ ) at  $Re = 100$ . All steady solutions are linearly stable unless indicated otherwise.

### 3.2. Radial confinement effects

Having considered the role of injection depth on the unconfined swirling jet's behaviour, we now proceed to studying the influence of radial confinement  $C$ . Here, branch continuations are performed with varying  $S$  and  $C$  at a Reynolds number of  $Re = 100$  (as above), and two fixed values of the injection depth:  $L = 2$  and  $L = 0$ . These  $L$  values correspond, respectively, to weakly and strongly axially confined situations.

#### 3.2.1. Weak axial confinement

As may be expected, for sufficiently weak levels of radial confinement (*i.e.*, sufficiently large values of  $C$ ), the evolution of the steady flow with  $S$  in the radially confined case closely matches the behaviour of the completely radially-unconfined flow considered above. For example, the  $C = 40$  solution curve in figure 3(a) is almost identical to the  $L = 2$  curve corresponding to  $C \rightarrow \infty$  from figure 2(a). In both cases, as  $S$  is increased at  $Re = 100$ , the flow develops a CRZ along a single-valued CJ solution curve without undergoing any bifurcations. As the radial wall is shifted inwards, however, figures 3(a) and (b) show that differences arise between the radially confined and unconfined jets' dynamics.

The first set of differences concerns the structure of the manifold of steady axisymmetric solutions. As the chamber diameter is decreased below  $C = 34.7$ , figure 3(b) indicates that the steady manifold becomes multivalued over a  $C$ -dependent interval of  $S$  values. Here, the same CJ topology as for  $C > 34.7$  persists, but an additional solution with an attached WJ topology appears in the state space. For example, note the disconnected solution curves at  $C = 16$  in figure 3(a). These CJ and WJ states are exemplified in figure 3(d) by the stagnation streamlines at points 2 and 4, respectively, and are separated by a saddle manifold solution



shown at point 3. We observe that the WJ state (figure 3(d) point 4) has a different structure in this radially confined context than is seen in the radially unconfined case. Here, the WJ manifests a large CRZ with a cone-shaped anterior that affixes to the radial wall rather than curling the jet backwards and attaching to the axial wall as in the radially unconfined case. Nonetheless, we believe that these observations can be interpreted using the same model proposed in section 3.1 of competing pressure gradients linked to centrifugal and Coandă effects. Though the presence of the radial wall has a strong influence on the apparent flow structure, we contend that the radial wall in this weakly axially confined flow serves the same purpose as the axial wall in the radially unconfined flow from section 3.1. Namely, in either case, the wall restricts entrainment, and its position controls the strength of the pressure deficit in the ORZ resulting from the Coandă effect.

The influence of this radial wall becomes even more prominent as the chamber diameter is further decreased below  $C \sim 12$ . For  $C \lesssim 12$ , the multivalued interval of  $S$  is dramatically shortened, such that the WJ state is single-valued at higher  $S$  values. Based on our interpretation, this decreased extent of the steady CJ solution manifold for  $C \lesssim 12$  implies that the Coandă effect-driven pressure deficit along the wall is beginning to overpower any centralising forces. For example, figure 3(a) shows that the steady CJ solution branch at  $C = 8$  terminates in a saddle–node bifurcation at  $S = 2.07$ , immediately after  $\min u_x(x, 0)$  crosses zero. As such, the WJ is the only steady solution branch identified for  $S > 2.07$  at  $C = 8$ . As  $C$  is further decreased, figure 3(b) shows that the transition to a WJ structure occurs at lower  $S$  values and that the  $S$  interval associated with multivaluedness shrinks. At the critical value  $C = 5.14$ , this dynamics manifests a codimension-2 cusp bifurcation at  $S = 1.99$  where the CJ and WJ solution branches meet. This means that there are no saddle–node bifurcations for  $C < 5.14$ , eliminating any concrete state space-based distinctions between CJ and WJ solutions. We attribute this behaviour to a strong relative dominance of the pressure gradient resulting from the Coandă effect in comparison to the pressure gradient acting to balance the centrifugal forces. For example, see the  $C = 4$  curve in figure 3(a). Moreover, differences in the physical appearance of CJ and WJ states also become ambiguous under such radially confined conditions. With  $C < 5.14$ , the axial location where the jet’s separation streamsurface attaches to the radial wall lies either before or approximately where the incipient CRZ first forms as  $S$  is increased. The stream does not separate from the radial wall in the wake of the CRZ. An example of this situation is visualised at the point  $(S, C) = (1.955, 4)$  in figure 3(e). As  $S$  is increased further, the CRZ enlarges, and the point where the jet impinges on the wall and the leading stagnation point of the CRZ both move upstream. The resulting flow pattern is shown at  $(S, C) = (2.3, 4)$  in figure 3(f). Overall, the breakdown process for such a strongly radially confined situation appears qualitatively more reminiscent of that in a vortex tube (e.g. Sarpkaya 1971) than that in a free jet.

The second set of differences concerns the presence of oscillatory non-axisymmetric instabilities that are not present in the radially unconfined jet at  $Re = 100$ . Such unsteady and three-dimensional behaviours are not a focus of this study, but are included in our results for completeness. At this  $Re$  value, figure 3(b) shows that Hopf bifurcations associated with  $|m| = 2$  eigenmodes appear in the  $(S, C)$  parameter plane as  $C$  is decreased from large values. At this Reynolds number, linear instabilities are almost entirely limited to the CJ flow regime. The instabilities themselves represent elongated, slowly co-rotating spiral structures concentrated along the jet shear layer with a frequency scaling that is approximately inversely proportional to the chamber’s cross-sectional area (i.e.  $f \sim 1/C^2$ ). Numerical continuation traced these neutral curves to the same bifurcations associated with subcritical co-rotating  $|m| = 2$  dynamics studied by Douglas *et al.* (2021) in the radially unconfined case. As shown in that paper, the nonlinear limit cycle oscillations manifested by these instabilities closely resemble the  $|m| = 2$  spirals described in the experiments of Billant *et al.* (1998).

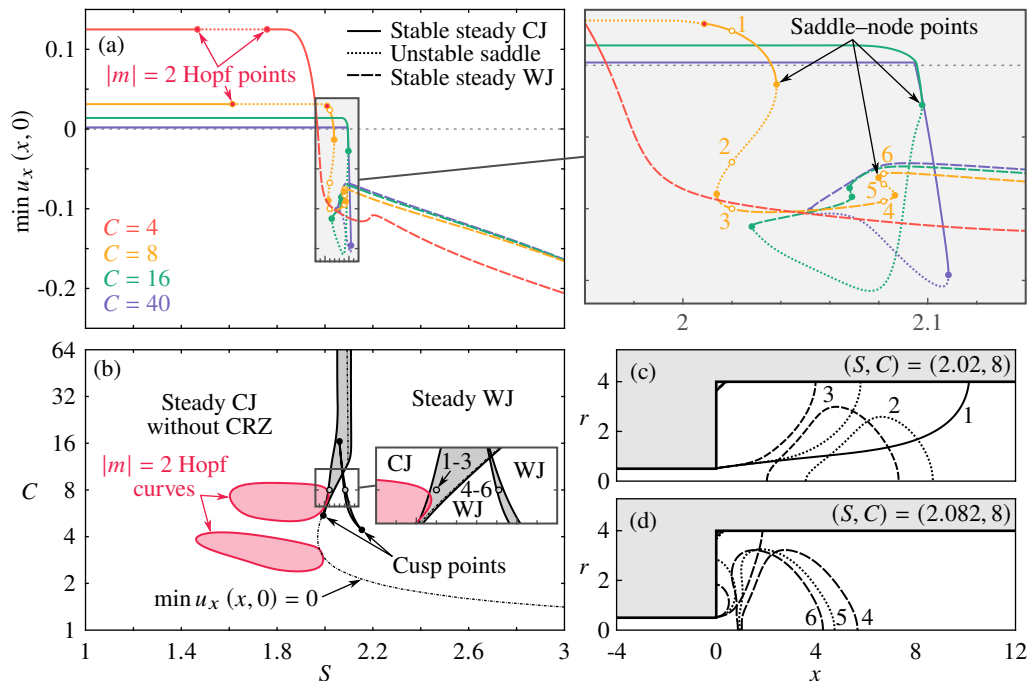


Figure 4: (a) Bifurcation diagrams, (b) stability map scaled logarithmically in  $C$ , and (c,d) streamline visualisations illustrating the effect of varying the chamber diameter and swirl ratio with strong axial confinement ( $L = 0$ ) at  $Re = 100$ . All steady solutions are linearly stable unless indicated otherwise.

Interestingly, this indicates that *axisymmetric* confinement by a radial wall can promote *non-axisymmetric* linear dynamics. Further analysis of these instabilities will not be pursued here, but could be an interesting direction for future work.

### 3.2.2. Strong axial confinement

Now we consider the effect of the chamber diameter parameter  $C$  on the steady dynamics of a flush-mounted jet ( $L = 0$ , strong axial confinement) at the same Reynolds number of  $Re = 100$ . As in section 3.2.2, figures 4(a) and (b) indicate that, for large enough  $C$  values (e.g.,  $C = 40$ ), the radially confined jet's bifurcation diagram converges to that of the radially unconfined jet with  $L = 0$  studied by Douglas *et al.* (2021) and recalled in figure 2(a). Hence, in this high- $C$  regime, the radial wall is not observed to have any significant effect, and the controlling role of axial confinement may be understood on the basis of the discussion in section 3.1. Likewise, the strong similarity between figures 4(b) and 3(b) for near-unity  $C$  indicates an opposite regime where the location of the axial wall has very little influence on the flow dynamics. In this case, it is the strong radial confinement that has a controlling influence on the flow structure, and the present flow's behaviour follows closely from the behaviours discussed in section 3.2.1 for  $C < 5.14$ .

The new and interesting behaviours observed for the radially confined jet with  $L = 0$  appear at intermediate  $C$  values, where the interplay between radial and axial confinement effects are significant. Consider the case of  $C = 8$ , whose bifurcation diagram with varying  $S$  is shown in figure 4(a). As before, a pair of saddle–node bifurcations appears near  $S \sim 2$  that mark where the flow exhibits bistability between a quasicolumnar CJ state and a WJ along the radial wall. Visualisations of these steady CJ and WJ states are shown in figure 4(c) at

points 1 and 3, respectively, and the intermediate saddle solution between these stable states is also shown at point 2. This bistable behaviour is nearly identical to what is observed for the  $C = 8$  case with weak axial confinement shown in figure 3(a). However, a notable difference in the dynamics appears as  $S$  is increased beyond this initial bistable regime. Namely, an additional pair of saddle–node bifurcations appears at  $S \sim 2.08$  where a second interval of bistability is observed. Visualisations of the flow in this parameter interval are presented in figure 4(d). Here, a nonlinear transition occurs between two steady WJ states: one where the jet is attached to the radial wall (shown at point 4) and another where it is attached to the axial wall (shown at point 6). These states are separated by the unstable saddle state included in figure 4(d) at point 5. Hence, at intermediate  $C$ , the radial WJ state only exists for a narrow range of  $S$  values, and the flow eventually transitions to a monostable axial WJ as  $S$  is increased. The effect of varying  $C$  on these dynamics is apparent from figure 4(b), where this secondary bistable regime is shown to only exist for  $4 \lesssim C \lesssim 16$ . Outside of this range, confinement effects are dominated either by the axial or radial wall as explained in the previous paragraph.

### 3.3. Reynolds number effects

For completeness, we have repeated the analyses from sections 3.1 and 3.2 at an increased Reynolds number of  $Re = 150$  to probe the interplay between viscosity and confinement. The steady regime diagrams resulting from these calculations are presented in figure 5. In all cases, the steady flow’s physical structure and state space topology remain qualitatively very similar to the  $Re = 100$  conditions studied above. However, it should be remarked that linear stability calculations indicated the presence of many Hopf bifurcations associated with non-axisymmetric, oscillatory modes within each parameter space at  $Re = 150$ . A detailed analysis of these instabilities is beyond the scope of this study, although their dynamics would be worthy of further investigation.

Instead, the focus here is toward the steady, axisymmetric solutions. Figure 5 shows stability maps for the flow at  $Re = 150$  that may be directly compared to the  $Re = 100$  results from figures 2(b), 3(b) and 4(b). In the radially unconfined case, displayed in figure 5(a), these results indicate that the injection depth required to avoid the multivalued regime for all  $S$  increases by a significant margin at higher Reynolds numbers. Similar conclusions may also be gleaned from the radially confined cases shown in figures 5(b) and (c), where the diagrams reveal that the value of  $C$  required for the flow to behave as in the radially unconfined case increases dramatically at this higher  $Re$  value. For context, consider a swirling jet apparatus with  $C = 64$  and  $L = 2$ . Even in this extreme configuration, the radial confinement is still seen to have a decisive influence on the possible flow states over a range of  $S$ .

Importantly, since the parameter extent of the bistable regime grows with increasing  $Re$ , the presence of the WJ state should not be attributed to strong viscous effects associated with low Reynolds numbers. Rather, the findings discussed here, albeit over a quite restricted range of  $Re$ , indicate that the nonlinear effects sustaining this multivaluedness actually become more significant as viscosity decreases. Within the framework our physical interpretation, this means that decreasing viscosity extends the parameter range over which the competing low pressure regions in the CRZ or ORZ can dominate the flow structure. This conclusion is also consistent with recent experimental evidence at much higher Reynolds numbers (Gupta *et al.* 2022).

## 4. Concluding remarks

This investigation characterises the effect of geometric confinement on the nonlinear dynamics of laminar swirling jets using numerical branch continuation and bifurcation analysis. It

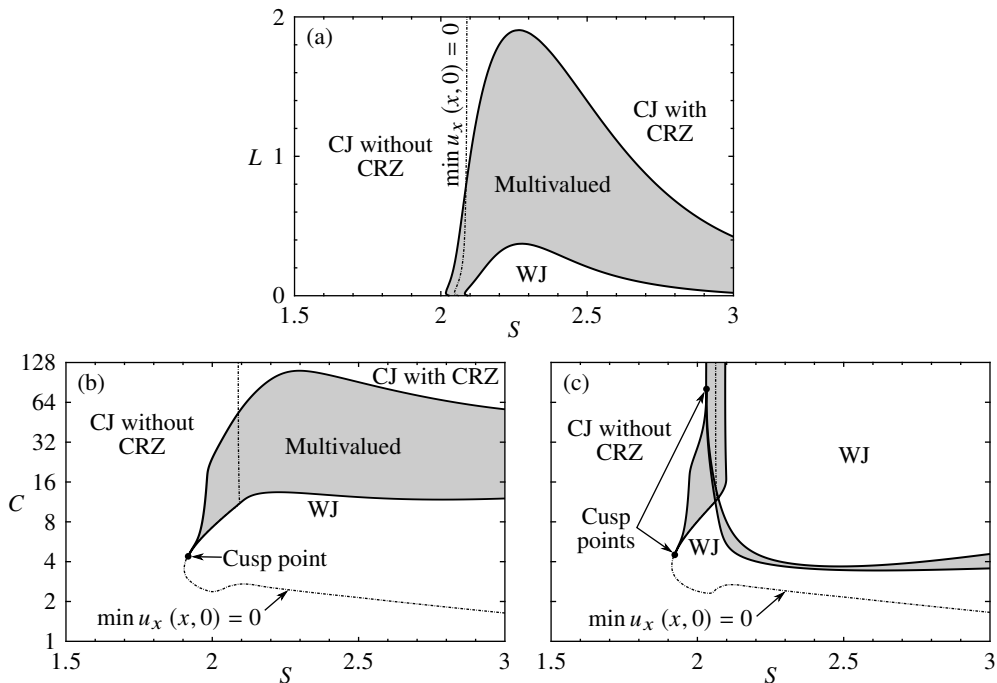


Figure 5: Steady regime diagrams at  $Re = 150$  for (a) the radially unconfined case ( $C \rightarrow \infty$ ), (b) the radially confined case with weak axial confinement ( $L = 2$ ), and (c) the radially confined case with strong axial confinement ( $L = 0$ ). (b,c) are scaled logarithmically in  $C$ . Note that instabilities (not indicated) are present over significant portions of the parameter space.

shows how the injection depth  $L$  and chamber diameter  $C$  affect the morphology of the jet's steady solutions under varying swirl amplitudes, and how confinement effects influence its underlying state space structure. This analysis is pursued by separately considering the role of  $L$  in a radially unconfined flow and the role of  $C$  in weakly and strongly axially confined jets. Overall, the swirling jet is shown to possess two basic types of dynamically distinct and, in some parameter regimes, bistable solutions that correspond to either quasicolumnar central jet (CJ) or noncolumnar wall jet (WJ) flow patterns. The flow in the CJ state does not interact strongly with flow boundaries and, depending on the parameters, may or may not exhibit a CRZ associated with vortex breakdown. Conversely, the WJ state is inextricably linked to interactions with flow boundaries through the Coandă effect and cannot appear in a completely unconfined situation.

The results of this study provide several new perspectives towards earlier reports. First and foremost, they quantify and highlight the immense sensitivity of swirling jets to confinement. As mentioned in section 1, earlier modelling efforts have already qualitatively demonstrated the sensitivity of swirling flows to radial boundary conditions (Ruith *et al.* 2004; Moise & Mathew 2019). Yet, such analyses have previously only linked this issue to relatively minor shifts in flow patterns, such as changes to the shape or position of the CRZ. On the other hand, many reports from experiments and computations have noted large-scale changes in the flow structure of swirling jets related to confinement but have largely focused on relatively strongly confined situations (Fu *et al.* 2005; Fanaca *et al.* 2010; Mohammad *et al.* 2011). The present study explains these observations and demonstrates how even weak confinement can completely alter the nature of the state space by allowing or disallowing

transitions between distinct attractors associated with fundamentally different patterns of flow. It also delineates the parameter regimes where such bistability can or cannot occur. From a practical perspective, such considerations reveal that it is unlikely that any closed experimental or engineering apparatus exists where a strongly swirling jet behaves as though it is truly unconfined for all conditions, even if a nonswirling jet within the same apparatus would. This point is particularly relevant for swirl-stabilised combustors, where the diametric expansion from the nozzle is typically characterised by a factor of  $O(1)$ . It should be recognised that such flows evolve in a quite strongly confined regime, and that results from unconfined simulations involving identical injector hardware may not even qualitatively apply to a confined application. Furthermore, these confinement-controlled state space differences certainly extend beyond the steady and axisymmetric regime studied here. As mentioned in section 3.2, our linear stability results suggest a notable influence of confinement upon the self-excited dynamics present in any given configuration. In a private discussion, our colleague J.-M. Chomaz pointed out that the Reynolds stress induced by laminar oscillations or turbulent flow conditions could interact in a significant way with the normal stresses induced by the centrifugal and Coandă effects highlighted throughout this paper. If this is indeed the case, such unsteady effects may cause a given mean flow state to differ substantially from the steady flow state corresponding to the same parameter values and initial conditions. Furthermore, as pointed out by a referee, it is plausible that transient effects related to such self-excited dynamics could induce intermittent CJ/WJ transitions near the bistability boundaries of the steady flow (analogous to the state-switching observed in reacting wakes by Suresha *et al.* (2016) and in non-reacting wakes by Grandemange *et al.* (2013)).

Additionally, this study calls into question the significance of the vortex breakdown phenomenon in regard to the widely reported hysteresis associated with confined jets under varying levels of swirl. Indeed, as in several earlier studies (Billant *et al.* 1998; Ruith *et al.* 2003; Ogus *et al.* 2016; Moise & Mathew 2019), this study finds the formation of a CRZ to occur via a smooth, non-critical process with increasing  $S$ . Though axisymmetric vortex breakdown is certainly associated with hysteresis in inviscid columnar vortex flows (Wang & Rusak 1997a), available theory also suggests that the expansion associated with a swirling jet flow could destroy this hysteretic behaviour (Rusak *et al.* 1997), as could its viscosity (Wang & Rusak 1997b) or its particular velocity profile (Leclaire & Sipp 2010). Instead, our results suggest that it is a competition between low pressure regions in the CRZ and ORZ, and not strictly vortex breakdown, that control the bistable behaviour of axially and/or radially confined laminar swirling jets. We believe this idea is supported by other experiments and simulations available in the literature. For example, Billant *et al.* (1998) have described hysteresis between “cone breakdown” and “bubble breakdown” states in their experiments, as have Liang & Maxworthy (2005). By accounting for the degree of confinement associated with their apparatuses and comparing their visualisations with our results, it seems quite clear that the bubble and cone states reported by these authors correspond to our CJ and WJ states, respectively. The same is more obviously true of the observations by Fu *et al.* (2005) and Vanierschot & van den Bulck (2007), who recognised the influence of the wall in the hysteresis behaviour described in their reports. Hence, we feel that the term “cone breakdown” is somewhat unsuitable, as this paper has argued that the WJ state is controlled by the Coandă effect through interactions of the jet with confinement rather than by the usual mechanisms of vortex breakdown, even though a CRZ remains present. In our view, identifying such solutions as WJ states provides a more direct reference to the dominant physics and provides a clear connection between similar states across confined and unconfined configurations. This explanation also holds for numerical studies employing simplified models of swirling jets (e.g. Moise & Mathew 2019; Keeton *et al.* 2022), where Dirichlet conditions imposed along the upstream boundary induce a similar competition between central and outer low

pressure regions and give rise to “wide-open cone” solutions that are analogous to the WJ. This suggests a very different conclusion compared to the recent criterion proposed by Keeton *et al.* (2022), which interpreted the transition to “cone breakdown” as a *local* effect controlled predominantly by the properties of the incoming jet fluid. Our results, in contrast, indicate that the transition between CJ and WJ states is influenced dramatically by interactions with the entrained fluid surrounding the jet.

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## REFERENCES

- BENJAMIN, T. BROOKE 1962 Theory of the vortex breakdown phenomenon. *Journal of Fluid Mechanics* **14** (4), 593–629.
- BERAN, PHILIP S. & CULICK, FRED E. C. 1992 The role of non-uniqueness in the development of vortex breakdown in tubes. *Journal of Fluid Mechanics* **242**, 491–527.
- BILLANT, PAUL, CHOMAZ, JEAN-MARC & HUERRE, PATRICK 1998 Experimental study of vortex breakdown in swirling jets. *Journal of Fluid Mechanics* **376**, 183–219.
- BROWN, G. L. & LOPEZ, J. M. 1990 Axisymmetric vortex breakdown part 2. physical mechanisms. *Journal of Fluid Mechanics* **221**, 553–576.
- DOUGLAS, CHRISTOPHER M., EMERSON, BENJAMIN L. & LIEUWEN, TIMOTHY C. 2021 Nonlinear dynamics of fully developed swirling jets. *Journal of Fluid Mechanics* **924**, A14.
- DOUGLAS, CHRISTOPHER M., EMERSON, BENJAMIN L. & LIEUWEN, TIMOTHY C. 2022 Dynamics and bifurcations of laminar swirling annular jets. *Journal of Fluid Mechanics* (in press).
- FANACA, D., ALEMELA, P. R., HIRSCH, C. & SATTELMAYER, T. 2010 Comparison of the Flow Field of a Swirl Stabilized Premixed Burner in an Annular and a Single Burner Combustion Chamber. *Journal of Engineering for Gas Turbines and Power* **132** (7).
- FRITZ, J., KRÖNER, M. & SATTELMAYER, T. 2004 Flashback in a swirl burner with cylindrical premixing zone. *Journal of Engineering for Gas Turbines and Power* **126** (2), 276–283.
- FU, YONGQIANG, CAI, JUN, JENG, SAN-MOU & MONGIA, HUKAM 2005 Confinement effects on the swirling flow of a counter-rotating swirl cup. In *Turbo Expo: Power for Land, Sea, and Air*, , vol. 2, pp. 469–478.
- GALLAIRE, F. & CHOMAZ, J.-M. 2003 Instability mechanisms in swirling flows. *Physics of Fluids* **15** (9), 2622–2639.
- GALLAIRE, F. & CHOMAZ, J.-M. 2004 The role of boundary conditions in a simple model of incipient vortex breakdown. *Physics of Fluids* **16** (2), 274–286.
- GALLAIRE, F., ROTT, S. & CHOMAZ, J.-M. 2004 Experimental study of a free and forced swirling jet. *Physics of Fluids* **16** (8), 2907–2917.
- GALLAIRE, FRANCOIS, RUTH, MICHAEL, MEIBURG, ECKART, CHOMAZ, JEAN-MARC & HUERRE, PATRICK 2006 Spiral vortex breakdown as a global mode. *Journal of Fluid Mechanics* **549**, 71.
- GRANDEMANGE, M., GOHLKE, M. & CADOT, O. 2013 Turbulent wake past a three-dimensional blunt body. part 1. global modes and bi-stability. *Journal of Fluid Mechanics* **722**, 51–84.
- GUPTA, RAVI, GOHIYA, RAJAT, VEMPATI, CHANDAN, HEMCHANDRA, SANTOSH & PANDA, PRATIKASH 2022 Hysteresis and bi-stability in transversely excited swirling flows. In *Turbo Expo: Power for Land, Sea, and Air*.
- GYLLENRAM, W., NILSSON, H. & DAVIDSON, L. 2007 On the failure of the quasicylindrical approximation and the connection to vortex breakdown in turbulent swirling flow. *Physics of Fluids* **19** (4), 045108.
- HALL, M. G. 1972 Vortex breakdown. *Annual Review of Fluid Mechanics* **4** (1), 195–218.

- HECHT, F. 2012 New development in FreeFem++. *Journal of Numerical Mathematics* **20** (3-4), 251–265.
- JIANG, TSUNG LEO & SHEN, CHIH-HUNG 1994 Numerical predictions of the bifurcation of confined swirling flows. *International Journal for Numerical Methods in Fluids* **19** (11), 961–979.
- KEETON, BENJAMIN W., CARPIO, JAIME, NOMURA, KEIKO K., SÁNCHEZ, ANTONIO L. & WILLIAMS, FORMAN A. 2022 Vortex breakdown in variable-density gaseous swirling jets. *Journal of Fluid Mechanics* **936**, A1.
- LECLAIRE, BENJAMIN & SIPP, DENIS 2010 A sensitivity study of vortex breakdown onset to upstream boundary conditions. *Journal of Fluid Mechanics* **645**, 81–119.
- LEIBOVICH, SIDNEY 1984 Vortex stability and breakdown - survey and extension. *AIAA Journal* **22** (9), 1192–1206.
- LIANG, HANZHUANG & MAXWORTHY, T. 2005 An experimental investigation of swirling jets. *Journal of Fluid Mechanics* **525**, 115–159.
- LIEUWEN, TIM, McDONELL, VINCE, SANTAVICCA, DOMENIC & SATTELMAYER, THOMAS 2008 Burner development and operability issues associated with steady flowing syngas fired combustors. *Combustion Science and Technology* **180** (6), 1169–1192.
- LOISELEUX, THOMAS & CHOMAZ, JEAN-MARC 2003 Breaking of rotational symmetry in a swirling jet experiment. *Physics of Fluids* **15** (2), 511–523.
- LOPEZ, J. M. 1994 On the bifurcation structure of axisymmetric vortex breakdown in a constricted pipe. *Physics of Fluids* **6** (11), 3683–3693.
- MANOHARAN, KIRAN, FREDERICK, MARK, CLEES, SEAN, O’CONNOR, JACQUELINE & HEMCHANDRA, SANTOSH 2020 A weakly nonlinear analysis of the precessing vortex core oscillation in a variable swirl turbulent round jet. *Journal of Fluid Mechanics* **884**, A29.
- MOHAMMAD, B. S., CAI, J. & JENG, SAN-MOU 2011 Gas Turbine Combustor Flow Structure Control Through Modification of the Chamber Geometry. *Journal of Engineering for Gas Turbines and Power* **133** (9).
- MOISE, PRADEEP & MATHEW, JOSEPH 2019 Bubble and conical forms of vortex breakdown in swirling jets. *Journal of Fluid Mechanics* **873**, 322–357.
- OBERLEITHNER, K., SIEBER, M., NAYERI, C. N., PASCHEREIT, C. O., PETZ, C., HEGE, H.-C., NOACK, B. R. & WYGNANSKI, I. 2011 Three-dimensional coherent structures in a swirling jet undergoing vortex breakdown: stability analysis and empirical mode construction. *Journal of Fluid Mechanics* **679**, 383–414.
- OGUS, G., BAELMANS, M. & VANIERSCHOT, M. 2016 On the flow structures and hysteresis of laminar swirling jets. *Physics of Fluids* **28** (12), 123604.
- O’CONNOR, JACQUELINE & LIEUWEN, TIM 2012 Recirculation zone dynamics of a transversely excited swirl flow and flame. *Physics of Fluids* **24** (7), 075107.
- RUITH, M.R., CHEN, P. & MEIBURG, E. 2004 Development of boundary conditions for direct numerical simulations of three-dimensional vortex breakdown phenomena in semi-infinite domains. *Computers and Fluids* **33** (9), 1225–1250.
- RUITH, M. R., CHEN, P., MEIBURG, E. & MAXWORTHY, T. 2003 Three-dimensional vortex breakdown in swirling jets and wakes: direct numerical simulation. *Journal of Fluid Mechanics* **486**, 331–378.
- RUSAK, Z. & JUDD, K. P. 2001 The stability of noncolumnar swirling flows in diverging streamtubes. *Physics of Fluids* **13** (10), 2835–2844.
- RUSAK, Z., JUDD, K. P. & WANG, S. 1997 The effect of small pipe divergence on near critical swirling flows. *Physics of Fluids* **9** (8), 2273–2285.
- SARPKAYA, TURGUT 1971 On stationary and travelling vortex breakdowns. *Journal of Fluid Mechanics* **45** (3), 545–559.
- SQUIRE, H.B. 1960 Analysis of the ‘Vortex Breakdown’ Phenomenon: Part I. *Tech. Rep. No. 102*. Imperial College of Science and Technology, Aeronautics Department.
- SURESHA, SUHAS, SUJITH, R. I., EMERSON, BENJAMIN & LIEUWEN, TIM 2016 Nonlinear dynamics and intermittency in a turbulent reacting wake with density ratio as bifurcation parameter. *Physical Review E* **94**, 042206.
- SYRED, NICHOLAS 2006 A review of oscillation mechanisms and the role of the precessing vortex core (PVC) in swirl combustion systems. *Progress in Energy and Combustion Science* **32** (2), 93–161.
- TAMMISOLA, O. & JUNIPER, M. P. 2016 Coherent structures in a swirl injector at Re=4800 by nonlinear simulations and linear global modes. *Journal of Fluid Mechanics* **792**, 620–657.
- VANIERSCHOT, M. & VAN DEN BULCK, E. 2007 Numerical study of hysteresis in annular swirling jets with a stepped-conical nozzle. *International Journal for Numerical Methods in Fluids* **54** (3), 313–324.
- VANIERSCHOT, M. & VAN DEN BULCK, E. 2009 Computation of a drastic flow pattern change in an annular

- swirling jet caused by a small decrease in inlet swirl. *International Journal for Numerical Methods in Fluids* **59** (5), 577–592.
- WANG, S. & RUSAK, Z. 1997a The dynamics of a swirling flow in a pipe and transition to axisymmetric vortex breakdown. *Journal of Fluid Mechanics* **340**, 177–223.
- WANG, S. & RUSAK, Z. 1997b The effect of slight viscosity on a near-critical swirling flow in a pipe. *Physics of Fluids* **9** (7), 1914–1927.
- WANG, SHIXIAO, RUSAK, ZVI, GONG, RUI & LIU, FENG 2016 On the three-dimensional stability of a solid-body rotation flow in a finite-length rotating pipe. *Journal of Fluid Mechanics* **797**, 284–321.
- ZHANG, YUXIN, RUSAK, ZVI & WANG, SHIXIAO 2019 Influence of inlet flow profiles on swirling flow dynamics in a finite-length pipe. *Physical Review Fluids* **4**, 014701.